

## Aqueous Quinoline Treatment with Iron/ Copper Activated UV/ Persulfate Process in a Falling Film Photo-Reactor

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### Abstract

This article reports the application of the homogenous UV/ persulfate process, activated with iron copper ions, for the treatment of quinoline (Qu) in aqueous solutions. A photo-reactor with a radial falling solution film around the UV lamp was utilized. Under established optimum conditions of  $[Qu]_0 = 40$  mg/L,  $[PS] = 1000$  mg/L, pH 6,  $[Fe^{2+}] / [Cu^{2+}] = 1$  mg/L and after 70 min, 88.3%, 94.8% and 96.4% degradations were achieved with UV/PS, UV/PS/ $Fe^{2+}$  and UV/PS/ $Cu^{2+}$  processes, respectively. Accordingly, total organic carbon (TOC) removals were 31.2%, 36.1% and 82.2% after 120 min, which highlights the amazing power of copper ions in the treatment. For each case, pseudo first order reactions were obtained for the used processes. The required irradiation energy per cubic meter of aqueous solutions was 127.6, 100.5 and 71.8 kWh for the used processes, respectively. Meanwhile, the role of active radicals was investigated using radical scavengers of ethanol and tert-butyl alcohol, indicating about 48.9% contribution of sulfate radicals in the degradation mechanism.

**Keywords:** UV/ Persulfate, Quinoline, Falling Film Reactor, Kinetic, Energy Consumption

### 1. Introduction

Many persistent and highly toxic hazardous materials are present in wastewaters from chemical factories. Quinoline (Qu) is a heterocyclic nitrogen compound that is used as a raw material and a solvent in the manufacturing of dyes, paints, herbicides and other fine chemicals [1]. It is also used for the production of many antiseptics, antibiotics and pharmaceuticals [2, 3]. Further, it exists in coal tar, mineral oil and petroleum wastewaters [4, 5]. With an N-heteroatom incorporated in the ring system,

Qu has higher solubility in water than its homo-cyclic analogs and can easily be transferred in soils, sediments and aquifer materials; consequently, it appears as a contaminant, especially in close landfills [6, 7]. Hence, Qu is hardly biodegradable, tends to huddle in natural water environments and exhibits toxic properties [8].

The well-known advanced oxidation processes (AOPs) are promising techniques for oxidative dissolution and mineralization of many organics in waters and wastewaters. AOPs are based on the generation of very reactive species such as  $HO^\bullet$  radicals that quickly oxidize a broad range of organic

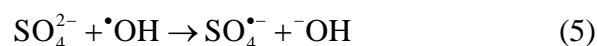
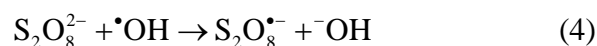
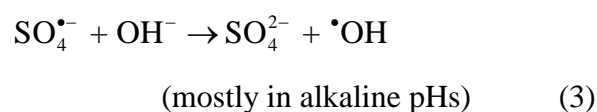
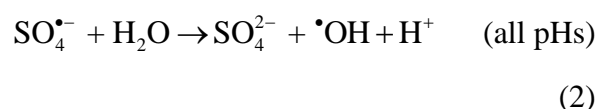
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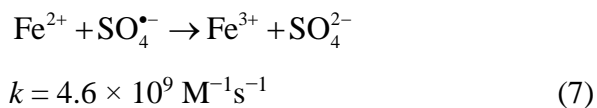
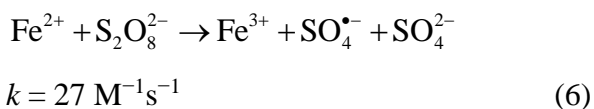
pollutants [9, 10]. Although advanced oxidation processes (AOPs) using  $O_3$  [11] and  $H_2O_2$  [12] have shown good performances in wastewater remediation, they frequently exhibit high running costs and other drawbacks [13, 14].

Due to the excellent properties of persulfate (PS) anion and the lower price of its salts, growing attention has been paid over recent years to utilizing different processes with this reagent. It is also used for in situ chemical oxidation (ISCO) to transform groundwater or soil contaminants into less harmful chemical species [15]. PS salts dissociate in water to the PS anion ( $S_2O_8^{2-}$ ) which is kinetically slow in reacting with many organics [16]; however, it has been well established that it can be photo-chemically or thermally activated to generate sulfate radical ( $SO_4^{\bullet-}$ ) [17, 18], which is a stronger oxidant (redox potential 2.6 V) with a kinetically fast reacting tendency with organic pollutants in contaminated waters. PS is normally available as a salt associated with ammonium, sodium or potassium. Previous works have reported that potassium persulfate (KPS) gives better results in photo oxidative removal of some organic materials than other PS salts under natural pH [9]. PS is usually activated by heat [19], UV light [20], bases [21], soil minerals [22] and radiolysis [23] as well as transition metals ( $Fe^{2+}$  and  $Cu^{2+}$ ) [24, 25] to form sulfate radicals. In soils and groundwater, the sulfate radicals are free to react with a wide range of contaminants which can further generate other reactive species, such as hydroxyl radicals ( $\bullet OH$ ), peroxymonosulfate ( $HSO_5^-$ ) and hydrogen peroxide ( $H_2O_2$ ) [22] that are

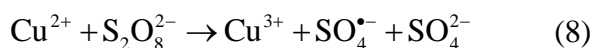
vital in degrading organic pollutants in water and soil. Briefly, generation of the radicals has been described via the following reactions [9, 18]:



In this process, sulfate ions are produced which may lead to an increase in salt content in the effluent; however, this case does not seem to be a serious problem, because there are no legal restrictions on sodium/potassium sulfate in wastewaters [18, 26]. Accordingly, transition metal ions, especially ferrous metals, have been proven to be efficient PS activators [24]. Ferrous ions can rapidly activate PS to form sulfate radicals ( $SO_4^{\bullet-}$ ) at a high rate constant of  $k = 27 \text{ M}^{-1}\text{s}^{-1}$ . However, the high reduction potential of  $Fe^{2+}$  ions and the high redox potential of the generated sulfate radicals may initiate an even stronger but not favorable, scavenging reaction of sulfate radicals by  $Fe^{2+}$  ions ( $k = 4.6 \times 10^9 \text{ M}^{-1}\text{s}^{-1}$ ) [19]. Ferrous ions are converted simultaneously by both PS ion and sulfate radicals and the final reaction product ( $SO_4^{2-}$ ) remains in the system. The reactions are [19]:



Similarly,  $\text{Cu}^{2+}$  ions activate PS to form sulfate radicals and sulfate ions. Nevertheless, study in copper to activate PS has received little attention [27]. Copper ions can be oxidized to  $\text{Cu}^{3+}$  as [28]:



Leading to copper ions being generated to contribute in the oxidation of pollutants and give more efficiency compared to activation with iron ions [24].

No attempt has been made so far for the photodegradation treatment of Qu in the presence of PS. This study attempts to investigate using UV/PS for the treatment of Qu by means of a high performance and low energy consumption photo-reactor with solution falling film device. The influencing parameters of contaminant initial concentration, pH, oxidant concentration, as well as iron and copper ions activator dosages are evaluated. From TOC analysis, the extent of the substrate mineralization is followed. Also, the role of active radicals is studied using radical scavengers of ethanol (EtOH) and tert-butyl alcohol (t-BuOH). Further, the reactions kinetic are investigated and the consumed irradiation energy is evaluated for each of the used processes.

## 2. Experimental

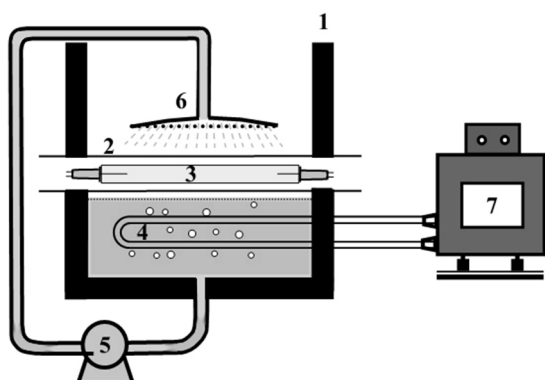
### 2-1. Materials

All reagents were used as received without further purifications. Quinoline,  $\text{C}_9\text{H}_7\text{N}$  ( $\geq 97\%$ ), MeOH (HPLC grade),  $\text{CH}_3\text{COOH}$  (HPLC grade), EtOH (99.9%) and t-BuOH ( $> 99\%$ ),  $\text{K}_2\text{S}_2\text{O}_8$  (99%),  $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$  (99.5%) for supplying  $\text{Fe}^{2+}$  ion,  $\text{CuSO}_4 \cdot 5\text{H}_2\text{O}$  (99%) for  $\text{Cu}^{2+}$  ion,  $\text{H}_2\text{SO}_4$  (98%), NaOH ( $\geq 97\%$ ) were all Merck products. All solutions were made up in deionized water with conductivity less than  $0.08 \mu\text{S}/\text{cm}$ .

### 2-2. Reactor set-up and procedure

Experiments were performed in a stainless steel rectangular cubic reactor (Fig. 1). The interior dimensions were 23 cm length, 7 cm width and 21 cm depth. The amount of solution in this reactor was about one liter, leveled at about 2 cm below the horizontal quartz tube. The light source was a UV-C (6 W, Philips) which was located horizontally in a quartz tube (2.5 cm diameter) at the center of the reactor. The content of the reactor was circulated by a pump, so that the solution was sprayed via a liquid distributor over the quartz tube, forming a film around the quartz tube perimeter. By exposure to light, most degradation reactions are expected to perform in this region, where mass transfer has the minimum resistance. The contacted solution film entered the bulk, leveled just below the quartz tube. The solution after facing the coil in the bulk entered the suction point of the pump. The device therefore facilitated the solution to expose the UV light over each circulation path. The reactor was equipped with a stainless steel coil, containing a water flow from an external

thermostat bath to regulate the reactor temperature with an accuracy of  $\pm 0.1$  °C.



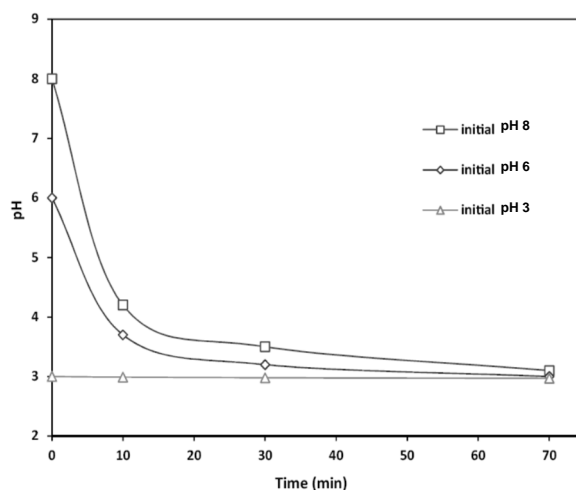
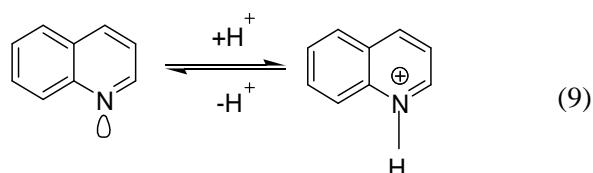
**Figure 1.** The used photo-reactor setup; 1: reactor, 2: quartz tube, 3: UV lamp, 4: temperature regulating coil, 5: pump, 6: distributor, 7: thermostat.

To perform each experiment, a solution (1 L) with an initial concentration of Qu (within 20-60 mg/L) was prepared. The pH was adjusted to the desired value by means of a pH meter (Denver, UB-10) using dilute  $\text{H}_2\text{SO}_4$  (0.1 M) or  $\text{NaOH}$  (0.1 M) solutions and after addition of KPS (corresponding to desired PS ion concentration), the solution was transferred into the reactor. To initiate the process, the lamp was turned on and samples (3 mL) were withdrawn at regular times to analyze the Qu concentration. All experiments were conducted at 25°C, as the most conventional environmental temperature.

### 2-3. Analytical method

The Qu concentration in each sample was analyzed with a UV-Vis spectrophotometer (Jasco, V-630), measuring the absorbance at  $\lambda_{\text{max}} = 312$  nm joined with a calibration curve and in agreement with the Beer-Lambert's

law (absorbance less than 1.3). As was mentioned in introduction section, reactions between PS and most organic pollutants are slow; however, with the effect of UV light, PS ions decompose into active sulfate radicals which in turn speed up the oxidation process. The generation of sulfate radicals is accompanied by the  $\text{H}^+$  generation (Eqs. 1-3) and consequently, as can be seen in Fig. 2, pH of the solution decreases. Under this condition, Qu molecules tend to react with  $\text{H}^+$  ions and develop protonated form (Eq. 9) which has a higher light absorbance ability due to  $\text{H}^+$  ion bonding with N lone pair electrons [29].

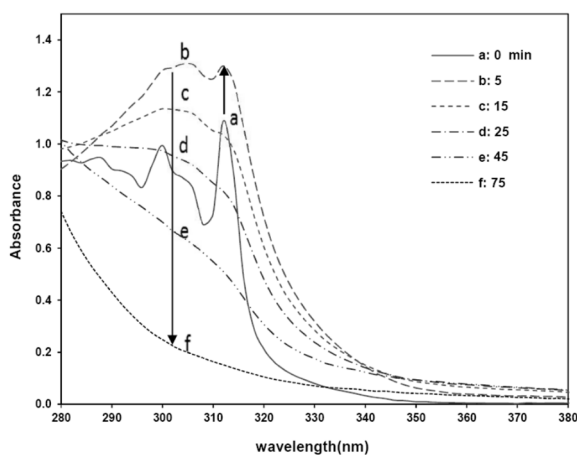


**Figure 2.** Variation of solution pH during UV/PS process with different initial pH values:  $[\text{Qu}]_0 = 40$  mg/L and  $[\text{PS}] = 1000$  mg/L.

The UV-Vis spectra (Fig. 3) shows that the UV absorbance at  $\lambda_{\text{max}}$  rises in the first 5 minutes; then it decreases during the remaining process time. Accordingly, the

process was considered in degradation mode of Qu just after this first 5 minutes of reaction progress. By measuring the initial absorption ( $A_0$ ) and at any time ( $A_t$ ) of the solution at  $\lambda_{max}$ ; the extent of contaminant degradation efficiency ( $X$ ) was calculated as:

$$X = \frac{A_0 - A_t}{A_0} \quad (10)$$



**Figure 3.** UV-Vis spectrum of Qu at different times of UV/PS process:  $[Qu]_0 = 40$  mg/L,  $[PS] = 1000$  mg/L and pH 6.

Consequently, optimization of the process was aimed, based on the obtained  $X$  values, but other important complementary analysis were also employed.

Because of different intermediates produced during the degradation process and in order to examine the interference in the UV-Vis absorption at  $\lambda_{max}$ , the only Qu concentration was followed via the HPLC peaks joined with the relevant calibration curve. The HPLC equipment (SYKAM, Germany) was equipped with a column (Nucleosil C18,  $4.6 \times 250$  mm) and UV spectrophotometer as a detector and the mobile phase was a mixture of 30% methanol and 70% (pH 5.5, 50 m

acetic acid + 8% methanol) flowing with a rate of 1mL/min. The HPLC peak of Qu appears at the retention time of 20.40 min [30]. After determining Qu concentration, the specific degradation efficiency was obtained from Eq. (10), unless the initial,  $[Qu]_0$  and any time,  $[Qu]_t$  concentrations (in mg/L) were substituted with the amounts of HPLC absorbance. The efficiencies based on HPLC and UV-Vis analysis methods are very close (maximum difference of about 7% at Qu degradation efficiency of about 37%) and approach the same values after about 70 min. This closeness indicates that UV-Vis analysis is reliable to follow Qu concentration at different times. Previous studies on Qu degradation with AOP methods of wet oxidation process and UV/TiO<sub>2</sub> process [31-33] indicate formation of nicotinic and picolinc acids and 2(1H)-quinolinone intermediates which have different  $\lambda_{max}$ .

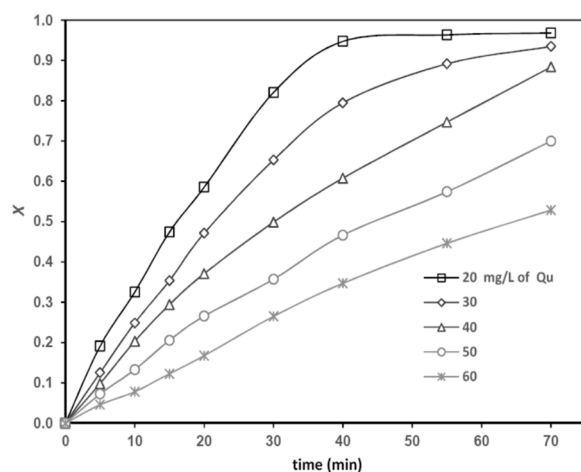
Furthermore, the total organic carbon (TOC) of samples was measured (under optimum conditions) by means of a TOC meter (multi, N/C 3100, Germany) and similarly, the initial and any time TOC values (in mg/L) were used to determine the extent of substrate mineralization.

### 3. Results and discussion

#### 3-1. Effect of substrate initial concentration

Various Qu initial concentrations, from 20 to 60 mg/L with a PS concentration of 1000 mg/L and under natural pH of near 6 were examined. The considered range of Qu in this work is within the range used by other investigators [32-34]. As presented in Fig. 4, degradation efficiency decreases with initial Qu concentration. Having a constant amount of reactive reagent with the light intensity as

well as PS amount, a decrease in degradation efficiency is expected with higher substrate dosages; however, as is obvious, degradation efficiency was not significant when initial concentration increased from 20 to 40 mg/L (8.7% difference after 70 min). This implies that 40 mg/L initial Qu concentration is representative.

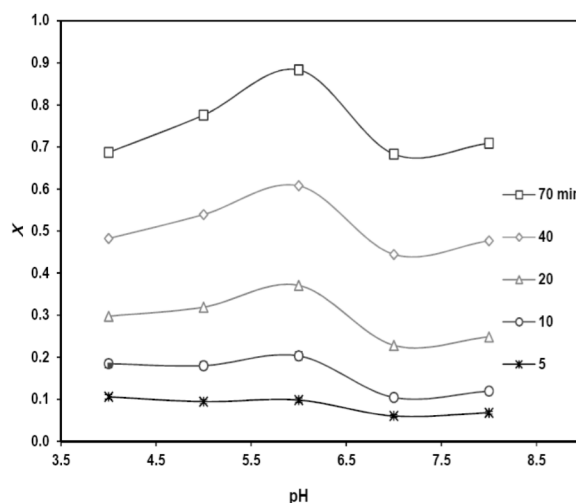


**Figure 4.** Effect of initial Qu concentration on its degradation efficiency: [PS]= 1000 mg/L and pH 6.

### 3-2. Effect of solution pH

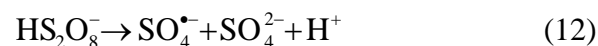
The pH dependency of the UV/PS process, under typical initial PS concentration of 1000 mg/L is depicted in Fig. 5. The efficiency gradually decreases with either an increase or a decrease in pH with respect to the solution natural pH of 6. Similar trends of variations have been previously reported for pollutants degradation via activated PS [20, 35]. Under alkaline conditions,  $\text{SO}_4^{\bullet-}$  species undergo reactions with  $\text{OH}^-$  to generate  $\bullet\text{OH}$  radicals according to Eq. (3). Despite conversion of  $\text{SO}_4^{\bullet-}$  to  $\text{SO}_4^{2-}$  and producing  $\bullet\text{OH}$  radicals with the redox potential of 2.8 V [36] which is slightly more than redox potential of  $\text{SO}_4^{\bullet-}$  (2.6 V), extra amounts of  $\text{SO}_4^{2-}$  ions can

inactivate  $\bullet\text{OH}$  and  $\text{SO}_4^{\bullet-}$  species, since  $\text{SO}_4^{2-}$  at high concentrations can perform as  $\bullet\text{OH}$  radical scavenger (Eqs. 2 and 3) [37].



**Figure 5.** Effect of pH on degradation efficiency:  $[\text{Qu}]_0 = 40$  mg/L and  $[\text{PS}] = 1000$  mg/L.

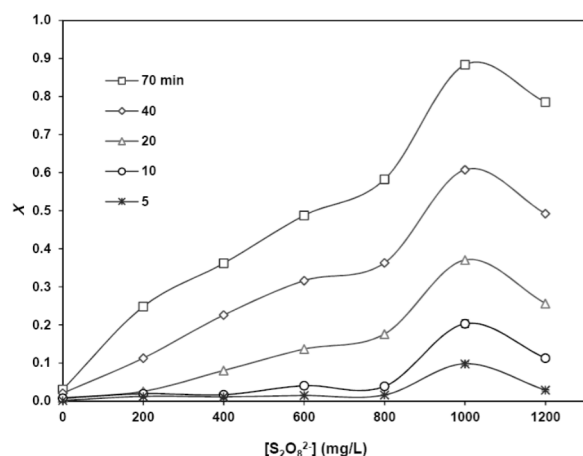
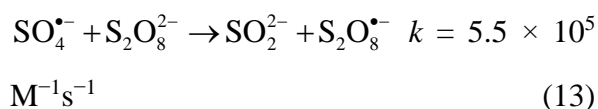
On the other hand, applying acidic conditions leads to additional generation of  $\text{SO}_4^{\bullet-}$  radicals, according to the following equations [17]:



which in turn, may cause radical with radical reactions instead of radical with pollutant [38]. It is noteworthy, according to Eqs. (2 and 3), that  $\text{H}^+$  is released while  $\text{OH}^-$  is consumed. So, the solution pH is decreased as the reaction proceeds. Considering the highest level of degradation, obtained at natural initial pH of 6 and privileges of applying mild conditions, this pH can be introduced as the optimum for the process.

### 3-3. Effect of persulfate initial concentration

The initial concentration of  $S_2O_8^{2-}$  was found to be an important parameter for the degradation of Qu in the UV/PS process. As is demonstrated in Fig. 6, increase of PS, up to about 1000 mg/L, causes the efficiency to improve due to more reactive radical generation. However, as reported in previous studies [9,39], increase in the PS concentration could not continuously ensure an improvement in the pollution removal since PS itself is a scavenger of  $SO_4^{\bullet-}$ , indicated by the following equation:



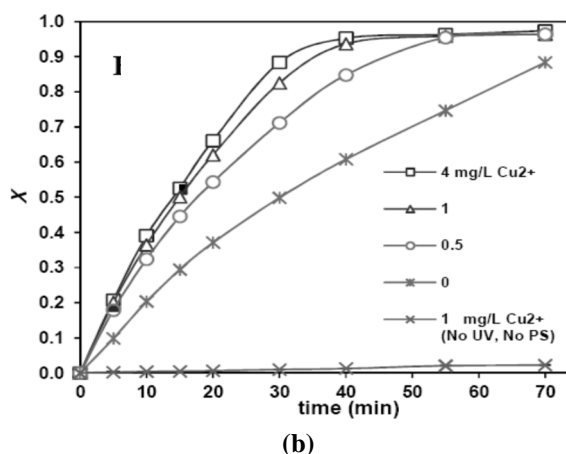
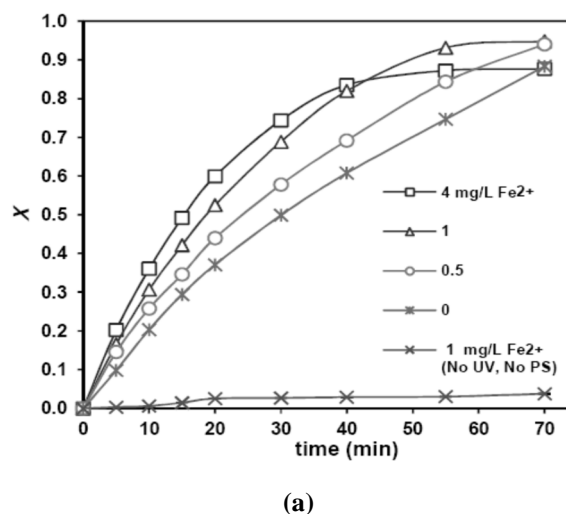
**Figure 6.** Effect of oxidants concentration on degradation efficiency:  $[Qu]_0 = 40$  mg/L and pH 6.

Hence, the optimal value for PS is about 1000 mg/L at which a high efficiency of 88.3% can be achieved after 70 min treatment.

### 3-4. Process intensification with $Fe^{2+}$ and $Cu^{2+}$ ions

Further activation of PS reagent was examined using different concentrations of

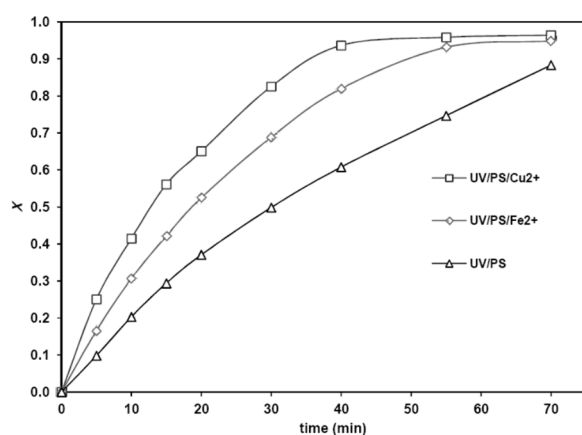
$Fe^{2+}$  and  $Cu^{2+}$ , within 0.5–4 mg/L. Fig. 7 A shows that in the UV/PS/ $Fe^{2+}$  process, Qu undergoes a more efficient degradation compared with UV/PS process. This confirms that, according to Eqs. (6, 7),  $Fe^{2+}$  ions accelerate PS activation to form sulfate radicals  $SO_4^{\bullet-}$  and therefore improved degradation efficiency. In this regard, 1 mg/L of  $Fe^{2+}$  was found to be the optimum dosage. Higher  $Fe^{2+}$  dosages can act as an effective scavenger of sulfate radicals, therefore, a balance between generation and consumption of sulfate radicals appeared in the presence of higher amounts of  $Fe^{2+}$  ions [24,40].



**Figure 7.** Effect of iron (a) and copper (b) concentrations on degradation efficiency:  $[Qu]_0 = 40$  mg/L,  $[PS] = 1000$  mg/L and pH 6.

In UV/PS/Cu<sup>2+</sup> process, Cu<sup>2+</sup> ions give a continuous enhancement in degradation during the reaction period. As indicated by Eq. (8), Cu<sup>3+</sup> species are generated which, despite its unstable state, may act as an oxidant for Qu degradation [24]. Using 1 mg/L, of copper ion provides about 93.7% of Qu degradation in less than 40 min and higher dosage gives no more promotion (Fig. 7b). So, similar to Fe<sup>2+</sup>, 1 mg/L can be introduced as the optimum Cu<sup>2+</sup> concentration. Also, it can be observed in Fig. 7 (a and b) that the metal ions alone (with no UV and no PS) do not provide any degradation.

Depicted in Fig. 8 is a comparison between three conducted processes; among them, UV/PS/Cu<sup>2+</sup> shows the most effective degradation (93.7% compared to 60.8% with UV/PS and 81.9% UV/PS/Fe<sup>2+</sup>, all after 40 min). It must be mentioned that applying just UV light irradiation or PS without UV light irradiation (darkness) does not provide any degradation for Qu.

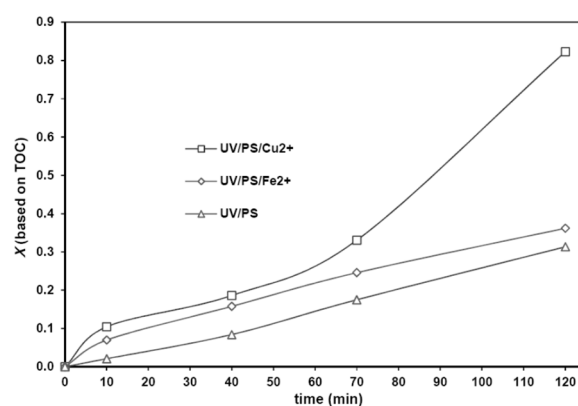


**Figure 8.** Qu degradation with different processes: [Qu]<sub>0</sub>= 40 mg/L, [PS]= 1000 mg/L, [Fe<sup>2+</sup>]= 1 mg/L, [Cu<sup>2+</sup>]= 1 mg/L and pH 6.

### 3-5. Mineralization assessment

Organics due to the mineralization will be

converted to CO<sub>2</sub> and H<sub>2</sub>O and TOC criterion indicates the extent of conversion of carbons and heteroatoms into inorganic species. For UV/PS, UV/PS/Fe<sup>2+</sup> and UV/PS/Cu<sup>2+</sup> processes, under the mentioned optimum conditions TOC measurements were performed at different times and corresponding efficiency based on initial and any time TOC values were obtained. As is presented in Fig. 9, interestingly, UV/PS/Cu<sup>2+</sup> process provides the highest TOC efficiency more than double of the other processes, elevates significantly within 70-120 min and reaches to 82.2% mineralization. Such a sharp increase is not observed for the other two processes. The reason can be discussed in terms of copper activity which results in a continuous degradation not only with Qu but also with intermediates throughout the reaction period [24].



**Figure 9.** Comparison of TOC removal for the used processes: [Qu]<sub>0</sub>= 40 mg/L, [PS]= 1000 mg/L, [Fe<sup>2+</sup>]= 1 mg/L, [Cu<sup>2+</sup>]= 1 mg/L and pH 6.

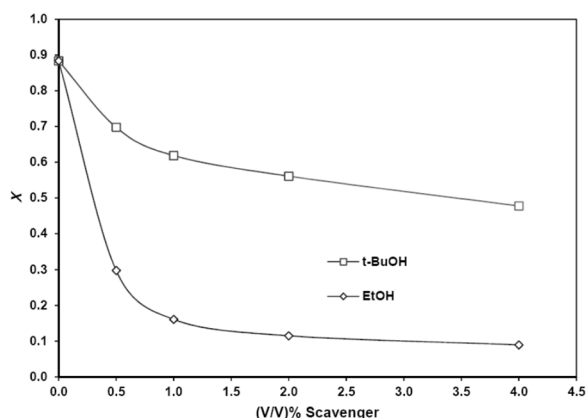
### 3-6. The role of radical oxidizing species in degradation mechanism

Degradation of organic pollutants by PS reagent is generally considered to occur upon reaction with SO<sub>4</sub><sup>•-</sup> and •OH oxidizing reagents. To determine their contribution in



Qu degradation, two alcohol radical scavengers, EtOH and t-BuOH, were used to capture reactive species during the process. EtOH can quench both hydroxyl and sulfate radicals whereas t-BuOH reacts mainly with hydroxyl radicals and poorly with sulfate radicals [41]. The difference in the extent of progress with the scavengers can therefore represent the sulfate radicals contribution in degradation.

The influence of using alcohols is presented in Fig. 10 for a typical time of 70 min. EtOH has decreased the efficiency much more than t-BuOH. Adding 4% (V/V) of EtOH or t-BuOH, for instance, has caused a 8.9% and 47.7% decrease in efficiency, respectively, compared to normal operations. These observations imply that both radical species are effective in the degradation process and the average contribution of hydroxyl and sulfate radicals is obtained about 51.1% and 48.9%, respectively.



**Figure 10.** Influence of scavengers in UV/PS process after 70 min:  $[Qu]_0 = 40$  mg/L,  $[PS] = 1000$  mg/L and pH 6.

Qu degradation in the presence of hydroxyl radicals leads to the formation of three major intermediates: pyridine-2-carboxylic acid (picolinic acid), pyridine-3-carboxylic acid

(nicotinic acid) and 2(1H)-quinolinone [31-33]. It is thought that similar to hydroxyl radicals, an oxidation–reduction reaction occurs by sulfate radicals and organic compounds can be decomposed. Both  $\cdot OH$  and  $SO_4^{\cdot -}$  are electrophilic species that usually attack the positions with higher electron density. The formation of the first formed intermediates may depend on the electrophilic substitution between Qu and  $\cdot OH$  as well as Qu and  $SO_4^{\cdot -}$ . The initial oxidation mainly occurs at positions 5 and 8 of the aromatic ring, resulting in the formation of 5,8-quinolinedione. In the continuity, considering that the electron cloud density of the pyridine ring is lower than that of the aromatic ring, the pyridine ring is relatively difficult to be oxidized and the cleavage occurs in the aromatic ring. The reactions then occur consecutively to generate picolinic and nicotinic acids. In another parallel branch, hydroxyl radicals may react with Qu and at the C-2 position of the pyridine ring [31-33] leading to generate 2(1H)-quinolinone. The decomposition continues by ring opening to final steps of mineralization. The nitrogen content in the Qu converts to ammonia or nitrate ions species.

### 3-7. Kinetic study

Due to the practical applications, the kinetic degradation of Qu was investigated with UV/PS, UV/PS/ $Fe^{2+}$  and UV/PS/ $Cu^{2+}$  processes under the optimum conditions of  $[PS] = 1000$  mg/L,  $[Fe^{2+}] = 1$  mg/L,  $[Cu^{2+}] = 1$  mg/L, pH 6,  $T = 25^\circ C$  and during 70 min for the two earlier processes. As was presented by Fig. 8, degradation proceeds to high levels with UV/PS/ $Cu^{2+}$  process and remains almost

constant after about 40 min. So, the kinetic of this process was considered within this period of time.

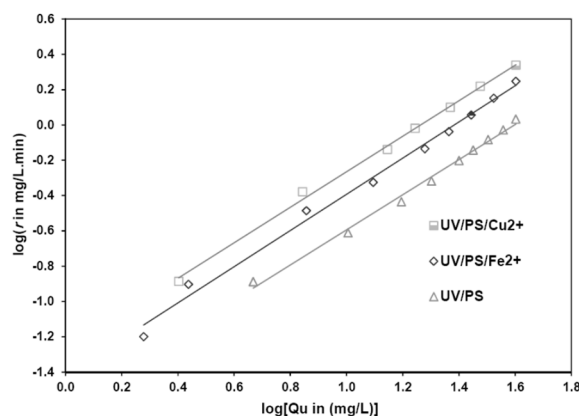
The utilized kinetic model is here the common power equation [42, 43]:

$$r = k [\text{Qu}]^n \quad (14)$$

Where  $r$ ,  $k$  and  $n$  denote rate, rate constant and order of the reaction, respectively. To obtain the appropriate kinetic parameters the differential method of data analysis based on the degradation rates calculated from Qu concentration variation versus time was used according to:

$$\log r = \log k + n \log[\text{Qu}] \quad (15)$$

The plots in Fig. 11 show good agreement of the experimental data with the above equation ( $R^2$  values close to unity). Kinetic parameters of the used processes together with the coefficients of determination are listed in Table 1. The results consistently show (within experimental error) pseudo first order reaction rates.



**Figure 11.** The kinetic diagram of the used processes:  $[\text{Qu}]_0 = 40$  mg/L,  $[\text{PS}] = 1000$  mg/L,  $[\text{Fe}^{2+}] = 1$  mg/L,  $[\text{Cu}^{2+}] = 1$  mg/L and pH 6.

**Table 1**

Kinetic parameters in different processes;  $[\text{Qu}]_0 = 40$  mg/L,  $[\text{PS}] = 1000$  mg/L,  $[\text{Fe}^{2+}] = 1$  mg/L,  $[\text{Cu}^{2+}] = 1$  mg/L and pH 6.

Process	n	k (mg/L) <sup>1-n</sup> /min	R <sup>2</sup>
UV/PS	0.99	0.030	0.997
UV/PS/Fe <sup>2+</sup>	0.99	0.038	0.992
UV/PS/Cu <sup>2+</sup>	1.00	0.053	0.993

### 3-8. Irradiation energy consumption

Dependency to the dose of UV light is vital since UV light is the main effective agent in The activation of KPS for producing hydroxyl and sulfate radicals in the reaction media. The photochemistry commission of the international union of pure and applied chemistry (IUPAC) has proposed a figure-of-merit (or more appropriately, an efficiency index, to compare electrical efficiency of different AOPs) for UV-based AOPs. It is a criterion of the irradiation efficiency in an AOP. It is defined (for low concentration of pollutants) as the electrical energy in kilowatt hours (kWh) required bringing about the degradation of a contaminant by one order of magnitude for 1 m<sup>3</sup> of contaminated solutions. Considering first-order degradation kinetics, the UV dose is calculated for each of the processes as [44]:

$$E_{EC} = \frac{1000 \times P \times t}{60 V \log(C_i / C_f)} \quad (16)$$

Where  $P$  is the lamp power (kW),  $t$  is the irradiation time,  $V$  is the solution volume (L) in the reactor and  $C_i$  and  $C_f$  are the initial and final pollutant concentrations. Considering the first-order degradation

kinetic for the decay of Qu concentration, the constant ratio of  $\ln(C_i / C_f) / t$  represents the rate constant,  $k$  (in  $\text{min}^{-1}$ ). The above equation can therefore be written as:

$$E_{EC} = \frac{38.4 \times P}{V \times k} \quad (17)$$

Thus, the required  $E_{EC}$  for the photochemical degradation of Qu solution with UV/PS, UV/PS/Fe<sup>2+</sup> and UV/PS/Cu<sup>2+</sup> was obtained as 127.6, 100.5 and 71.8 kWh/m<sup>3</sup>, respectively. Considering the electrical energy price in the U.S. market, 0.07 US\$/kWh (in 2014) [45], the electrical energy cost will be about 8.93, 7.03 and 5.02 US\$/m<sup>3</sup> for the used processes, respectively. The comparison, presented in Table 2, together with all relevant conditions shows that the process of UV/PS/Cu<sup>2+</sup> consumes much lower energy in Qu degradation.

**Table 2**

Comparison of energy consumption for degradation in different processes: [Qu]<sub>0</sub>= 40 mg/L, [PS]= 1000 mg/L, [Fe<sup>2+</sup>]= 1 mg/L, [Cu<sup>2+</sup>]= 1 mg/L and pH 6.

Process	EEC (kWh/m <sup>3</sup> )	Cost (US\$/m <sup>3</sup> )
UV/PS	127.6	8.93
UV/PS/Fe <sup>2+</sup>	100.5	7.03
UV/PS/Cu <sup>2+</sup>	71.8	5.02

#### 4. Conclusions

The activated persulfate by ultraviolet light and intensified with metal ions were successfully examined to degrade quinoline in homogenous reactions by means of a high performance radial falling film photo-reactor. The more important deduced aspects from this study are: i) the pertinent optimum conditions were: [Qu]<sub>0</sub>= 40 mg/L, [PS]=

1000 mg/L, [Fe<sup>2+</sup>]= 1 mg/L, [Cu<sup>2+</sup>]= 1 mg/L and natural pH of 6; ii) progress of the processes was not so sensitive to pH variations and naturally provided pH was effective; iii) under optimum conditions, for the three treatment processes of UV/PS, UV/PS/Fe<sup>2+</sup> and UV/PS/Cu<sup>2+</sup>, a substrate degradation around 90% was achieved after 70 min treatment; iv) mineralization assessment by TOC criterion indicated a wide advantage of using metal activators. Process intensifying with copper ions was revealed to generate much more efficient during short times; v) adding radical scavengers showed that both the sulfate and hydroxyl radicals were active with nearly half contribution from each, vi) pseudo first order reaction rates were relevant for the used three processes; and vii) the use of metal ions was shown to significantly save energy.

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